

to 1000 are being used. However, the breadboard is being constructed from commercial equivalents. The main board will be enclosed in a 30 mil aluminum box.

The breadboard employs an 8086 processor, 1Mb RAM and 64Kb ROM. An ACTEL FPGA handles memory access, error correction, data acquisition, spacecraft time, performs watchdog functions and interfaces with the RF transmitter/receiver. For flight the ACTEL A1280XL will be used. To facilitate prototyping two A1020s are being used instead.

The main board also performs analog signal conditioning for the payload magnetometer, temperature sensors and sun sensor. All of the analog data will be read by a 12-bit Analog-to-Digital converter.

In an effort to minimize power consumption the analog circuitry will be powered off about 90% of the time on a rapid cycling basis so that it will not affect data collection. Additionally the static processor and memory will be halted between data samples.

### 4.3 Magnetometer and Attitude Sensor

A 3-axis magnetometer will be accurately aligned relative to the spacecraft axes. The satellite will have been released with spin principally around the axis of the cylinder that is designed to have the largest moment of inertia. A damping mechanism will be included so that the spin will decay to rotation only around this axis. In order to determine the fields in absolute coordinates both the two angles defining the direction of the spin axis and the phase of the rotation must be known.

The direction of the spin axis can be determined by using the magnetometer and a sun sensor in combination and noting that the spin axis should remain fixed over an orbit. When the satellite is within  $\sim 2R_E$  of the earth the magnetic field is accurately known and only minimally variable. The magnetic field along the axis should remain constant as the satellite spins. The ratio of that field and the known magnitude of earth's field is the cosine of the angle between the spin axis and the field axis. The other two components will vary sinusoidally with the phase of the rotation angle. The maximum occurs in the plane defined by the magnetic field and spin axis directions. Using a sun sensor the phase of the rotation relative to the satellite-sun line can be determined and therefore the absolute direction of the satellite spin axis.

While it is reasonable to extrapolate that the spin axis remains fixed as the satellite moves around its orbit, it is not possible to know the spin rate with sufficient accuracy to determine the phase of the rotation at the time that a measurement is taken. Therefore, the sun sensor will be used while the magnetometer measurements are being made to determine the rotation phase angle.

The sun sensor will look radially outward from the satellite. It will consist of a slit and a sharply defined photodiode. We expect that the angular accuracies of the magnetic field measurements will be better than two degrees.

A flux-gate magnetometer will be utilized. A specific design has not been selected. However, Applied Physics Systems 553 has adequate sensitivity, weighs 20 grams and uses 200mW of power. Radiation hardness is not known but the fundamental flux-gate mechanism is insensitive to radiation. This system is strongly temperature sensitive,  $\sim 1nT/^{\circ}C$ . A temperature sensor and thermal compensation must be included. The circuitry is being designed for 0.5nT or 1% accuracy whichever is less stringent.

Historically, magnetic field sensitivity is attained by sufficient magnetic cleanliness on the spacecraft. While the fact that very little power

eliminating current loops. We anticipate considerable testing and adjustment of the mechanical properties of the electronics before being able to define a configuration and a magnetometer location.

### 4.4 Design Summary

Thus far neither satellite structure nor thermal balance have been considered in any detail. The mass of the structure will be estimated comparable to mass of the components. Some of the satellites can be eclipsed for up to four hours. We have included sufficient batteries to maintain electrical operation during this time. Thermal shielding will be required to maintain operating temperatures during this time.

The major power consuming component on the main board is the 12-bit ADC which in continuous operation requires 595mW. As mentioned above we plan to run this on a 10% duty cycle so that the power consumption will be cut to 60mW. Similarly some of the other components can be run on 10 or 20% duty cycles while others such as the clock must run continuously. Taking these factors into account the average power consumption on the main board will be 340mW. Based on the Applied Physics Systems magnetometer power consumption for continuous operation would be about 300mW. Average power consumption by the RF system is negligible since it is used for such a small fraction of the time. Thus the total average power consumption estimate is 640mW as compared to the 1W generated by the solar cells.

The mass of the components in the breadboard version of the main board have been weighed at 140g and the aluminum enclosure at 60g. The shielded solar cells weigh 40g and the magnetometer at 20g. The five AA equivalent batteries weigh 125g. The estimated weight of the RF system suggested above is 40g. Thus the total component mass is 325g. With an allowance for structure somewhat smaller than the component mass the total mass is under the 1kg target.

## 5. Satellite Launch and Release

Several vehicles were considered for launching the constellation into the final orbit. The best suited candidate was determined to be the Pegasus XL from Orbital Sciences Inc. Because of its relatively low cost, each plane could be launched on its own vehicle. If a larger launch vehicle were used, several plane changes would be required. The large fuel requirements for these burns could significantly reduce any gains in launch performance.

### 5.1 Launch Scenario

The launch sequence is made up of four steps that will end with the insertion of the satellites into a range of orbits. The first step is to use the Pegasus XL to launch the bus into a 200 km altitude circular parking orbit. At this time the bus will separate from the Pegasus and continue to the final orbit. Step two consists of a STAR 27E kick motor to raise apogee to  $5R_E$ . After the completion of this burn the STAR kick motor would be jettisoned and a hydrazine rocket would perform the remaining burns. The third step is a hydrazine burn that raises perigee to  $1.4R_E$ . The final burn occurs during the release of the satellites. A more detailed description is outlined below.

Using the Pegasus XL it is possible to lift 465 kg into a 200 km altitude parking orbit (Orbital Sciences, 1997). At this point the bus would separate from the Pegasus and continue to the final orbit. The separation mechanism standard on the Pegasus has a mass of 1 kg allowing the bus to have a mass of 453 kg. The change in velocity